Corporate Reserve of St. Charles

Sanitary Sewer Evaluation

Performed for

The City of St. Charles, Illinois



Performed by

Wills Burke Kelsey Associates, Ltd.



April 24, 2012

INTRODUCTION

On behalf of JCF Real Estate and the City of St. Charles, Wills Burke Kelsey Associates, Ltd. (WBK) has evaluated the impacts of the proposed land use change within the Corporate Reserve of St. Charles project. Impact evaluation is related to the City of St. Charles wastewater collection system. The Corporate Reserve site is located in St. Charles west of Randall Road and north of IL Route 64, near the intersection of Woodward Drive and Corporate Reserve Boulevard. Original development concepts anticipate primarily office use with some commercial use along IL 64. Two single story office buildings have been constructed and a site prepared for a third. JCF is proposing to change a majority of land use from office to high density residential. Based on a Concept Site Plan submitted by JCF Real Estate on March 21, 2012, the proposed development consists of 331 rental units and a club area on approximately twenty acres. JCF Real Estate is interested in connecting to the City of St. Charles wastewater collection system and receiving wastewater treatment service from the City of St. Charles West Side Wastewater Treatment Plant. This report considers existing conditions of the sanitary sewer which includes the potential for future development to be serviced by the existing sanitary system, and assesses the impact to the sanitary sewer as a result of land use changes and increased flows from the proposed Corporate Reserve development.

SCOPE OF EVALUATION

The system components to be evaluated as part of this study include three sanitary sewer pipe networks and the Renaux Manor Lift Station. If it is found that these components can facilitate flows and are within the original design capacities, future evaluation of downstream force main and gravity sewer is not warranted.

The first pipe network is the trunk sanitary sewer that extends from the Renaux Manor Lift Station (just east of the intersection of Peck Road and Campton Hills Road), north along Peck Road to Voltaire Lane. The second pipe network is the existing collection system along Woodward Drive, which begins along Cardinal Drive, flows west along Woodward Drive, and into the Peck Road trunk sewer. A connection into this system from the Corporate Reserve improvements is proposed along Cardinal Drive. The third sanitary sewer pipe network is within the Remington Glen subdivision. This system is tributary to the Woodward Drive collection system and a connection into this system from the Corporate Reserve development is also proposed. This portion of the City's wastewater collection system includes pipe ranging in size from 8 inches to 15 inches in diameter.

All three sanitary sewer systems were evaluated utilizing a simplified approach considering flowing full capacity based on manning's equation. Two different wet weather flow regimes were considered; with and without proposed flows from Corporate Reserve. Conservatively,

we did not evaluate dry weather flows because wet weather conditions will be most critical and the "minimum" flow condition that the system must be able to handle. A spreadsheet was developed to determine the capacity of representative pipe segments in the network and tributary flows to each segment. In addition to existing sites tributary to the system, future development bound by Woodward Drive and IL Route 64 was identified and considered in the evaluation. The collection system to be evaluation also includes the lift station at Renaux Manor. The Renaux Manor Lift Station was initially evaluated based on a comparison of existing and projected flows to the original design flows and calculations. Additionally, pump run time provided by the City of St. Charles was reviewed and compared to flow estimates.

PIPE CAPACITY ANALYSIS

The first component of the evaluation was to determine the capacity of the existing pipe network. All areas tributary to the collection system were identified and considered. Sanitary sewers pipes range in size from 8 to 15 inches in diameter and all sewers were constructed with relatively new subdivisions and commercial developments that were built starting in the mid 1990's. The pipe slopes, sizes, lengths, rim elevations, and invert elevations utilized in the analysis were determined from the following sources:

- Remington Glen Record Drawings, prepared by Cowhey Gudmundson Leder, Ltd., dated 09/20/05
- Record Plans for Final Engineering Renaux Manor and the Towns of Renaux Manor Unit 1, prepared by Wiseman-Hughes Enterprises, dated 08/18/99
- Record Drawings Grading Improvements Phase II The Corporate Reserve of St. Charles, prepared by Mackie Consultants LLC, dated 03-29-11
- City of St. Charles GIS Data, provided by the City of St. Charles
- Renaux Manor Sanitary Sewer Mains, Lift Station, and Force Main Record Drawings, prepared by Intech Consultants, INC., dated 4/21/97

Detailed sanitary sewer information for all three pipe networks is located on Exhibit 1 in the Appendix.

Design Flow Determination for Capacity Analysis

A capacity analysis was performed for all three sanitary sewer pipe networks. Two wet weather conditions flow regimes were considered:

- Existing (without Corporate Reserve development); and
- Proposed (with Corporate Reserve development)

It should be noted the "Existing" flow regime includes all existing conditions as well as undeveloped parcels which will be served by the system under evaluation. All lots tributary to each network were included and flows were input at select manholes. Inflow and infiltration was added at the upstream manhole of all pipe networks at 500 gal/in/mi/day. Supporting calculations can be found in the Appendix.

Remington Glen subdivision is serviced by a sanitary sewer pipe network with pipe sizes ranging from 8 to 12 inches in diameter. Based on the approved Illinois Environmental Protection Agency (IEPA) Water Pollution Control Permit, a total of 26 multiple dwelling units were estimated to generate a total of 36,050 gallons per day (gpd).

The existing collection system that runs along Cardinal Drive, and extends west along Woodward Drive before connecting to the Peck Road trunk system was evaluated based on the existing development serviced by the system and potential future development on the three vacant lots bound by IL Route 64 to the south and Woodward Drive to the north. Existing development tributary to the system includes office buildings at Corporate Reserve, Main Street Center, Autumn Leaves Assisted Living, and Remington Glen subdivision. Approved IEPA Water Pollution Control permits yielded an average daily flow rate of 6,000 gpd and 3,200 gpd at the assisted living facility and Main Street Center, respectively. Wastewater flows for the Corporate Reserve office buildings were estimated based on a wastewater generation rate of 15 gpd/employee. The number of employees was calculated based on one employee per 250 square feet of office space. Future wastewater generation rates for the three vacant lots were conservatively calculated using a population equivalent (PE) of 20 per acre of land.

Land uses tributary to the trunk system along Peck Road include single family homes (Renaux Manor Unit 1, Renaux Manor Unit 3 and Artesian Springs), multi-family homes (Renaux Manor Unit 2), and commercial space (Valley Springs Auto, Westgate, and Walgreens). Approved IEPA Water Pollution Control permits for Valley Springs Auto, Westgate, and Walgreens were used to estimate the respective wastewater flows. Flows for the single and multi-family homes were estimated using the IEPA waterwater average daily flow generation rates. For single family homes, a rate of 350 gallons/household/day was used. For multi-family homes, all units were conservatively estimated to be 3 bedroom units with a rate of 300 gallons/unit/day. A total of 152 households in Renaux Manor Unit 1 and Artesian Springs are tributary to the system. 117 single family homes in Renaux Manor Unit 2.

The Renaux Manor Lift Station receives flow from the sanitary sewer trunk line along Peck Road, which is the collector for both the sanitary sewer system that serves the Remington Glen subdivision and the system along Woodward Drive. The lift station also accepts wastewater flow from tributary land uses to the east. These tributary areas include 35 multi-family units

from Renaux Manor Unit 2, Pine Ridge and Regency Estates (includes Aldi), The Bike Rack & adjacent commercial, the assisted living facility and St. Charles Fire Station No. 3. As mentioned above, wastewater generation rates were estimated at 300 gallons/unit/day for the multi-family units. The approved IEPA rate for Pine Ridge and Regency Estates was used, and flow rates for The Bike Rack & adjacent commercial, and the fire station were based on one employee for every 250 square feet of building, with an average daily use of 15 gpd/employee.

Based on the average daily flow, a peaking factor was calculated and applied in accordance with The Ten State Standards. The existing peak wet weather sanitary flow tributary to the Renaux Manor Lift Station is 1.155 cfs. The capacity analysis and peaking factor calculations for each manhole are shown in the Appendix on Exhibits 2 and 3 following this report. An exhibit showing the entire Renaux Manor Lift Station service area is also provided in Appendix A as Drawing OV1.

Results of Capacity Analysis

Based on the results of the capacity analysis, the pipe network can handle the existing condition wet weather flows. The existing conditions wet weather pipe capacity utilization ranges from 1% to 41% flowing full. Please note, our peak flow assumptions are conservative because all future development estimated at 20 PE per acre.

Next we looked at adding flows from the proposed land use changes at Corporate Reserve. Land use for the proposed development includes 15 buildings with a total of 331 rental units ranging from studios to two bedroom apartments. The percentage of studios, one bedroom, and two bedroom apartments in each building was estimated as shown on Exhibit 4 in the Appendix. Based on the calculated percentages, it was estimated that the average building includes 1 studio, 11 one bedroom apartments, and 10 two bedroom apartments. Using the IEPA waterwater average daily flow generation rates, a value of 4750 gpd was calculated for each building. This calculation can be found in Appendix A.

Based on the Preliminary Utility Plan for Corporate Reserve of St. Charles Phase II prepared by Mackie Consultants on 03-09-12, sanitary sewer is proposed to enter the existing pipe network in two locations. The collection system for Remington Glen will accept 0.375 cfs of additional peak flow from 20 buildings at manhole 6.4062. The remaining 0.062 cfs from 2 buildings will discharge into manhole 6.3194 along Cardinal Drive. After including flow from these additional 22 multi-family homes, the pipe utilization for the proposed condition wet weather flow is estimated to range from 1% to 58% flowing full. The proposed capacity analysis and peaking factor calculations for tributary flows into each manhole are shown in the Appendix on Exhibits 5 and 6 following this report. The Preliminary Utility Plan is also in the Appendix and labeled as Exhibit 7.

It is our opinion that the existing system can convey the proposed condition wet weather flows.

RENAUX MANOR LIFT STATION EVALUATION

The second component of the evaluation was to determine the capacity of the Renaux Manor Lift Station. All tributary areas to the Renaux Manor Lift Station were identified and considered. Design flow rate calculations and rates were taken from *"The Renaux Manor Pump Station Calculations,"* prepared by Wiseman-Hughes Enterprises, revised March 16, 1998.

Per the calculations prepared by Wiseman-Hughes Enterprises, the Renaux Manor Lift Station is designed for an average daily flow of 400,000 gallons per day. The associated Renaux Manor Lift Station Calculations are provided in the Appendix as Exhibit 8. Based on a survey conducted by WBK with City of St. Charles Staff, there are no major operational problems associated with the lift station that suggest it cannot handle the existing flow. There are also no indicators that the lift station will not be able to handle an increased flow, as long as its design peak flow capacity is not exceeded.

WBK estimated the existing average daily flow prior to the connection of the proposed improvements at Corporate Reserve to be 316,723 gallons per day. Including proposed improvements at Corporate Reserve would add an additional average daily flow of 71,250 gallons per day, totaling 387,973 gallons per day. A breakdown of the calculated average daily flow rates are on Exhibit 9 in the Appendix. Therefore, since the total estimated average daily flow is less than the average design daily flow, no improvements are necessary.

Furthermore, based on pump run time data from the City, the average pump run time is 1.2 hours a day for the months of January 2012 to March 2012. This equates to an average daily flow of 99,360 gpd which is significantly less than our estimate average daily flow in the proposed condition of 316,723 gpd. Additionally, peak run time from the data is 3.7 hours a day, which equates to a flow of 306,360 gpd. Therefore, since the real time peak run time is also less than the estimate average daily flow in the proposed condition, it is our opinion that the lift station will be able to handle the additional flow.

Further, average daily flow for the existing conditions in addition to the proposed project are less than the design average daily flow at the Renaux Manor Lift Station. An email survey was also conducted by WBK with the City of St. Charles staff to determine operational condition and concerns. Results of the survey indicated that there are no major operational problems with the Renaux Manor lift station (aside from inoperable VFD's that are determined unnecessary, a panel view screen, and control circuit board memory backup battery holder that is loose). In regards to the sanitary sewer system, there are no known trouble spots in the existing collection system, nor are there any issues with the force main along Peck Road.

SUMMARY AND RECOMMENDATIONS

Based on our evaluation, the proposed land use changes in Corporate Reserve can be facilitated by the existing wastewater collection system as shown on the Preliminary Utility Plan submitted by Mackie Consultants on 3/09/12. A conservative approach was made by WBK to analyze the existing pipe system by including future development on vacant lots and estimating flows for unoccupied buildings that are currently connected to the collection system. Adding projected sanitary sewer flows into the existing system will increase the flow, however; in the fullest pipe will still have over 40% capacity available. Therefore, no improvements are necessary.

Since there are no known operational issues with the lift station to date and it has not reached its maximum operational capacity, WBK believes the Renaux Manor Lift Station will be able to handle the additional waterwater flow generated from the proposed land use change at Corporate Reserve.

Upstream Manhola	Dovision Martinie	Upstream Manhola Kire	Gewenteent Maritale Ros	Uppettern Inwert	Dowrities insert	Figs Size	Pipe Lingth	Pipe Singer	Overn	Tate
6.3296	6.31.06	768.28	768.58	194,32	794.12		122	1.04%	3.19	PVC
8.3298	6.1154	762.38	MLAI	764.30	212.08		320	0.43%	4.98	PVC
6.3234	6.0393	191.91	794.37	162.68	162.87		238	0.43%	20.14	Pric
6.2393	5,1189	784.87	784.29	761.87	761-45		28.	0.64%	11.59	
6.3189	6.3188	194.39	700.40	161.45	101.08		2.00	0.87%	22.84	745
6.2284	6.1132	782.48	775.44	141.04	718.49		118	0.42%	18.42	Pro
6.313Id	6.3180	275.61	112.68	754.48	758.76			0.42%	16.1.1	PVC
8.3130	6.3131	772.68	212.66	758.76	258.17			0.495	13.94	PVC
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6.1000	6.1125	756.39	106.68	754.00	75.41			0.77%	31.49	
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6.3304	6.3101							1125	22.66	
8,3901	1:0089						00	8.21%	30.38	1
7,3089	7.3088							1.95%	20.44	
7.5188	7.3087						_	1.62%	0.00	
13061	7,3080							1.10%	35.84	
7.3096	3.8081							1.87%	20.48	
7.3085	2.3084						1	4.17%	11.00	
7.3084	7.5088							4.62%	18.72	
Y.1080	2 solu						-	0.41%	10.06	1
7.8082	7 3081							0.103	18.14	
7.8065	7,3080							0.52%	14.52	1
			initary Sewer - Peck Roa							

		- 34	HILEY SEWER - PIECE KOAT	0 10 Kenaux Man	or Litt station					
Upstieurs Marinele	Downstream Manhole	ligetreart Manhola Bim	Downstream Manhols Risk	Uppliant inset	Dewritemant Inward	Pipe Sile	Paie Langth	Pas Sope	Depth	Type
1.4000	3.4016	PER DI		100.04	100.78		807	1.37%	8.77	PHC
7,4050	7.3080			104.47	100		100	0.30%	17.44	PHC
7.8080	7.3084		744.28		Annual Contractor	2.8	042	0.12%	19.05	PVC
7.3004	2,3053	- F44.28	142.97	104.04	TTLAT	123	425	0.34%	19.44	PVC.
1.3003	2,9681	193,87	104.44	123.45	742.68	18 1	23.0	0.15%	20.58	
7,3003	7.0004		120.54	111.00	TID 44	110	281	0.17%	18.72	
7.8091	7.3018	C10.00	142.78	223.AE	101.94	210	25.7	0.34%	UTM-	_
7.3058	7,3017	140.38	- 101.14	121.09	.723.83	1.83	257	0.30%	18.80	_
7,3667	2.8018	729.14	735.44	221.42	733.88	35	295	0.19%	12.72	_
1,8016	7.80	125,44	735.4m	100 M	750.88		296	0.29%	18.58	
1.8003	7.8N8		345.5.5	Conception and the local diversity of the loc	113.44		212	11.15%	19.28	_

Vantreen Manhale	Desenstresen Manhale	Vantream Manhels Rive	Downstream Marthele Ros	Vetream insert	Description and Insert	Par See	Parlingh	Post Name	Depth	Test
6.3110	5.1509				1000			1.09%	3.46	
6.1028	6.3108							1.10%	8.54	
6.31258	6.3107							11 40%	1.68	
4.8007	6.3106							1,50%	\$.15	
6.302%	6.4063							0.94%	2.34	
8.4063	8.4052							0.57%	8.90	
6.4062	7.4048							0.32%	13.49	
7.4549	7.4048				A COLOR OF THE OWNER OF			0.38%	14.70	
7.4048	1.4047							0.37%	14.00	
3.4047	7.4046				The second s			0.31%	13.29	
7.8048	1.4041							0.10%	15.44	
7,4045	13094							0.34%	17.43	
7.30%4	7,3090				the second second			0.41%	18.94	
3:3099	2.3094							0.97%	\$90	
7,3090	1.3091				The second second			3.85%	9.60	
1.8041	1.3090							8.40%	11.11	
17.307NJ	73083							0.80%	20.80	

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EXHIBIT 1

		EXISTI	NG CONDITI	ONS CAP	ACITY AN	IALYSIS -	CORPORA	TE RESERVI	E TO PECK R	OAD	
Upstream Manhole	Downstream Manhole	Upstream Elevation	Downstream Elevation	Pipe Length	Pipe Diameter	Pipe Slope	Pipe Capacity (CFS)	Cummulative Peak Sanitary Flow (CFS)	Total I & I (CFS)	Cummulative Wet Weather Flow (CFS)	Pipe Capacity (%)
6.3196	6.3198	766.10	764.10	122	8	1.64%	1.551	0.007	0.00360	0.011	0.7
6.3198	6.3194	764.10	762.68	329	8	0.43%	0.796	0.014	0.00360	0.018	2.2
6.3194	6.3193	762.68	761.87	188	8	0.43%	0.795	0.025	0.00360	0.028	3.5
6.3193	6.3189	761.87	761.45	66	8	0.64%	0.967	0.025	0.00360	0.028	2.9
6.3189	6.3188	761.45	761.06	129	8	0.30%	0.666	0.067	0.00360	0.071	10.6
6.3188	6.3192	761.06	759.49	378	8	0.42%	0.781	0.067	0.00360	0.071	9.1
6.3192	6.3190	759.49	758.74	188	8	0.40%	0.765	0.120	0.00360	0.124	16.2
6.3190	6.3191	758.74	758.27	95	8	0.49%	0.852	0.120	0.00360	0.124	14.5
6.3191	6.3200	758.27	756.90	309	8	0.44%	0.807	0.120	0.00360	0.124	15.3
6.3200	6.3105	756.90	755.81	153	8	0.71%	1.023	0.120	0.00360	0.124	12.1
6.3105	6.3104	755.95	754.16	53	8	3.38%	2.227	0.144	0.00360	0.148	6.6
6.3104	6.3103	754.16	752.19	63	8	3.13%	2.143	0.144	0.00360	0.148	6.9
6.3103	7.3089	752.19	748.53	114	8	3.21%	2.171	0.144	0.00360	0.148	6.8
7.3089	7.3088	748.53	746.70	94	8	1.95%	1.691	0.144	0.00360	0.148	8.8
7.3088	7.3087	746.70	745.11	87	8	1.83%	1.638	0.144	0.00360	0.148	9.0
7.3087	7.3086	745.11	742.24	147	8	1.95%	1.693	0.164	0.00360	0.168	9.9
7.3086	7.3085	742.24	740.40	80	8	2.30%	1.838	0.164	0.00360	0.168	9.1
7.3085	7.3084	740.40	736.98	82	8	4.17%	2.475	0.164	0.00360	0.168	6.8
7.3084	7.3083	736.98	731.72	114	8	4.61%	2.603	0.164	0.00360	0.168	6.4
7.3083	7.3082	731.72	731.15	69	12	0.83%	3.247	0.376	0.00590	0.382	11.8
7.3082	7.3081	731.15	730.77	99	12	0.38%	2.213	0.376	0.00590	0.382	17.2
7.3081	7.3080	730.77	730.20	112	12	0.51%	2.549	0.410	0.00590	0.416	16.3

EXISTING CONDITIONS CAPACITY ANALYSIS - REMINGTON GLEN SYSTEM INTO MH 7.3083 ALONG WOODWARD DRIVE

Upstream Manhole	Downstream Manhole	Upstream Elevation	Downstream Elevation	Pipe Length	Pipe Diameter	Pipe Slope	Pipe Capacity (CFS)		Total I & I (CFS)	Cummulative Wet Weather Flow (CFS)	Pipe Capacity (%)
6.3110	6.3109	748.79	747.56	114	8	1.08%	1.259	0.226	0.00230	0.228	18.1
6.3109	6.3108	747.56	746.07	125	8	1.19%	1.323	0.226	0.00230	0.228	17.2
6.3108	6.3107	746.07	745.57	126	8	0.40%	0.763	0.226	0.00230	0.228	29.8
6.3107	6.3106	745.57	742.99	162	8	1.59%	1.529	0.226	0.00230	0.228	14.9
6.3106	6.4063	742.99	741.70	137	8	0.94%	1.176	0.226	0.00230	0.228	19.4
6.4063	6.4062	741.70	740.50	129	8	0.93%	1.169	0.226	0.00230	0.228	19.5
6.4062	7.4049	735.18	734.99	87	12	0.22%	1.669	0.226	0.00230	0.228	13.6
7.4049	7.4048	734.99	734.30	180	12	0.38%	2.212	0.226	0.00230	0.228	10.3
7.4048	7.4047	734.30	734.14	43	12	0.37%	2.179	0.226	0.00230	0.228	10.5
7.4047	7.4046	734.14	733.62	167	12	0.31%	1.993	0.226	0.00230	0.228	11.4
7.4046	7.4045	733.62	733.02	184	12	0.33%	2.040	0.226	0.00230	0.228	11.2
7.4045	7.3094	733.02	732.75	114	12	0.24%	1.739	0.226	0.00230	0.228	13.1
7.3094	7.3090	732.75	732.16	132	12	0.45%	2.388	0.226	0.00230	0.228	9.5
7.3093	7.3092	746.22	745.07	118	8	0.97%	1.196	0.225	0.00230	0.228	19.0
7.3092	7.3091	745.07	740.60	116	8	3.85%	2.379	0.226	0.00230	0.228	9.6
7.3091	7.3090	740.60	737.63	85	8	3.49%	2.265	0.226	0.00230	0.228	10.1
7.3090	7.3083	737.63	731.72	202	12	2.93%	6.111	0.226	0.00230	0.228	3.7

EXISTING CONDITIONS CAPACITY ANALYSIS - PECK ROAD INTO RENAUX MANOR LIFT STATION

Upstream Manhole	Downstream Manhole	Upstream Elevation	Downstream Elevation	Pipe Length	Pipe Diameter	Pipe Slope	Pipe Capacity (CFS)		Total I & I (CFS)	Cummulative Wet Weather Flow (CFS)	Pipe Capacity (%)
7.4002	7.4050	730.98	729.79	307	8	0.39%	0.754	0.255	0.00890	0.263	34.9
7.4050	7.3080	725.47	725.15	108	15	0.30%	3.526	0.255	0.00890	0.263	7.5
7.3080	7.3034	725.15	724.84	142	15	0.22%	3.026	0.636	0.01480	0.651	21.5
7.3034	7.3033	724.84	723.47	401	15	0.34%	3.786	0.636	0.01480	0.651	17.2
7.3033	7.3032	723.47	722.89	320	15	0.18%	2.758	0.636	0.01480	0.651	23.6
7.3032	7.3031	722.89	722.40	281	15	0.17%	2.705	0.671	0.01480	0.686	25.3
7.3031	7.3018	722.40	721.99	257	15	0.16%	2.587	0.671	0.01480	0.686	26.5
7.3018	7.3017	721.99	721.42	292	15	0.20%	2.862	1.126	0.02910	1.155	40.4
7.3017	7.3016	721.42	720.88	291	15	0.19%	2.790	1.126	0.02910	1.155	41.4
7.3016	7.3015	720.88	720.33	290	15	0.19%	2.821	1.126	0.02910	1.155	41.0
7.3015	7.3053	720.33	719.44	312	15	0.29%	3.459	1.126	0.02910	1.155	33.4

EXISTING PEAK FLOW CALCULATIONS

EXHIBIT 3

Manhole 6.3196 Sanitary Sewe	Manhole 6.3196 Sanitary Sewer Peak Flow					
PE	10					
Peaking Factor	4.41					
Peak Flow (Million Gallons Per Day)	0.005					
Peak Flow (Gallons Per Day)	4613					
Flow (Gallons Per Minute)	3					
Flow (CFS)	0.007					

Manhole 6.3198 Sanitary Sewer Peak Flow					
PE	21				
Peaking Factor	4.38				
Peak Flow (Million Gallons Per Day)	0.009				
Peak Flow (Gallons Per Day)	9154				
Flow (Gallons Per Minute)	6				
Flow (CFS)	0.014				

Manhole 6.3194 Sanitary Sewe	Manhole 6.3194 Sanitary Sewer Peak Flow					
PE	37					
Peaking Factor	4.34					
Peak Flow (Million Gallons Per Day)	0.016					
Peak Flow (Gallons Per Day)	15881					
Flow (Gallons Per Minute)	11					
Flow (CFS)	0.025					

Manhole 6.3189 Sanitary Sewe	Manhole 6.3189 Sanitary Sewer Peak Flow					
PE	103					
Peaking Factor	4.24					
Peak Flow (Million Gallons Per Day)	0.044					
Peak Flow (Gallons Per Day)	43504					
Flow (Gallons Per Minute)	30					
Flow (CFS)	0.067					

EXISTING PEAK FLOW CALCULATIONS

EXHIBIT 3

Manhole 6.3192 Sanitary Sewe	Manhole 6.3192 Sanitary Sewer Peak Flow					
PE	187					
Peaking Factor	4.16					
Peak Flow (Million Gallons Per Day)	0.078					
Peak Flow (Gallons Per Day)	77601					
Flow (Gallons Per Minute)	54					
Flow (CFS)	0.120					

Manhole 6.3105 Sanitary Sewe	Manhole 6.3105 Sanitary Sewer Peak Flow				
PE	226				
Peaking Factor	4.13				
Peak Flow (Million Gallons Per Day)	0.093				
Peak Flow (Gallons Per Day)	93373				
Flow (Gallons Per Minute)	65				
Flow (CFS)	0.144				

Manhole 7.3087 Sanitary Sewer Peak Flow					
PE	258				
Peaking Factor	4.11				
Peak Flow (Million Gallons Per Day)	0.106				
Peak Flow (Gallons Per Day)	106000				
Flow (Gallons Per Minute)	74				
Flow (CFS)	0.164				

Manhole 7.3083 Sanitary Sewer Peak Flow					
PE	619				
Peaking Factor	3.92				
Peak Flow (Million Gallons Per Day)	0.243				
Peak Flow (Gallons Per Day)	242827				
Flow (Gallons Per Minute)	169				
Flow (CFS)	0.376				

Manhole 7.3081 Sanitary Sewe	Manhole 7.3081 Sanitary Sewer Peak Flow				
PE	679				
Peaking Factor	3.90				
Peak Flow (Million Gallons Per Day)	0.265				
Peak Flow (Gallons Per Day)	264843				
Flow (Gallons Per Minute)	184				
Flow (CFS)	0.410				

Manhole 7.3080 Sanitary Sewe	r Peak Flow
PE	1,088
Peaking Factor	3.78
Peak Flow (Million Gallons Per Day)	0.411
Peak Flow (Gallons Per Day)	410905
Flow (Gallons Per Minute)	285
Flow (CFS)	0.636

Manhole 7.3032 Sanitary Sewe	Manhole 7.3032 Sanitary Sewer Peak Flow					
PE	1,153					
Peaking Factor	3.76					
Peak Flow (Million Gallons Per Day)	0.433					
Peak Flow (Gallons Per Day)	433494					
Flow (Gallons Per Minute)	301					
Flow (CFS)	0.671					

Manhole 7.3018 Sanitary Sewer Peak Flow				
PE	2,033			
Peaking Factor	3.58			
Peak Flow (Million Gallons Per Day)	0.728			
Peak Flow (Gallons Per Day)	727910			
Flow (Gallons Per Minute)	505			
Flow (CFS)	1.126			

EXISTING PEAK FLOW CALCULATIONS

EXH	BIT	3
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Manhole 7.4002 Sanitary Sewe	r Peak Flow
PE	410
Peaking Factor	4.02
Peak Flow (Million Gallons Per Day)	0.165
Peak Flow (Gallons Per Day)	164508
Flow (Gallons Per Minute)	114
Flow (CFS)	0.255

Manhole 6.3110 Sanitary Sewe	r Peak Flow
PE	361
Peaking Factor	4.04
Peak Flow (Million Gallons Per Day)	0.146
Peak Flow (Gallons Per Day)	145757
Flow (Gallons Per Minute)	101
Flow (CFS)	0.226

nitary Sewer Peak Flow Tributary to Renaux Manor Lift Staton					
PE	1,134				
Peaking Factor	3.76				
Peak Flow (Million Gallons Per Day)	0.427				
Peak Flow (Gallons Per Day)	426883				
Flow (Gallons Per Minute)	296				
Flow (CFS)	0.660				



PROPOSED CONDITIONS CAPACITY ANALYSIS - CORPORATE RESERVE TO PECK ROAD											
Upstream Manhole	Downstream Manhole	Upstream Elevation	Downstream Elevation	Pipe Length	Pipe Diameter	Pipe Slope	Pipe Capacity (CFS)	Cummulative Peak Sanitary Flow (CFS)	Total & (CFS)	Cummulative Wet Weather Flow (CFS)	Pipe Capacity (%)
6.3196	6.3198	766.10	764.10	122	8	1.64%	1.551	0.007	0.00390	0.011	0.7
6,3198	6.3194	764.10	762.68	329	8	0.43%	0.796	0.014	0.00390	0.022	2.8
6.3194	6.3193	762.68	761.87	188	8	0.43%	0.795	0.087	0.00390	0.095	11.9
6.3193	6.3189	761.87	761.45	66	8	0.64%	0.967	0.087	0.00390	0.095	9.8
6.3189	6.3188	761.45	761.06	129	8	0.30%	0.666	0.130	0.00390	0.138	20.6
6.3188	6.3192	761.06	759.49	378	8	0.42%	0.781	0.130	0.00390	0.138	17.6
6.3192	6.3190	759.49	758.74	188	8	0.40%	0.765	0.183	0.00390	0.190	24.9
6.3190	6.3191	758.74	758.27	95	8	0.49%	0.852	0.183	0.00390	0.190	22.3
6.3191	6.3200	758.27	756.90	309	8	0.44%	0.807	0.183	0.00390	0.190	23.6
6.3200	6.3105	756.90	755.81	153	8	0.71%	1.023	0.183	0.00390	0.190	18.6
6.3105	6.3104	755.95	754.16	53	8	3.38%	2.227	0.207	0.00390	0.215	9.6
6.3104	6.3103	754.16	752.19	63	8	3.13%	2.143	0.207	0.00390	0.215	10.0
6.3103	7.3089	752.19	748.53	114	8	3.21%	2.171	0.207	0.00390	0.215	9.9
7.3089	7.3088	748.53	746.70	94	8	1.95%	1.691	0.207	0.00390	0.215	12.7
7.3088	7.3087	746.70	745.11	87	8	1.83%	1.638	0.207	0.00390	0.215	13.1
7.3087	7.3086	745.11	742.24	147	8	1.95%	1.693	0.226	0.00390	0.234	13.8
7.3086	7.3085	742.24	740.40	80	8	2.30%	1.838	0.226	0.00390	0.234	12.7
7.3085	7.3084	740.40	736.98	82	8	4.17%	2.475	0.226	0.00390	0.234	9.5
7.3084	7.3083	736.98	731.72	114	8	4.61%	2.603	0.226	0.00390	0.234	9.0
7.3083	7.3082	731.72	731.15	69	12	0.83%	3.247	0.438	0.00800	0.450	13.9
7.3082	7.3081	731.15	730.77	99	12	0.38%	2.213	0.438	0.00800	0.454	20.5
7.3081	7.3080	730.77	730.20	112	12	0.51%	2.549	0.847	0.00800	0.863	33.9

PROPOSED CONDITIONS CAPACITY ANALYSIS - REMINGTON GLEN SYSTEM INTO MH 7.3083 ALONG WOODWARD DRIVE

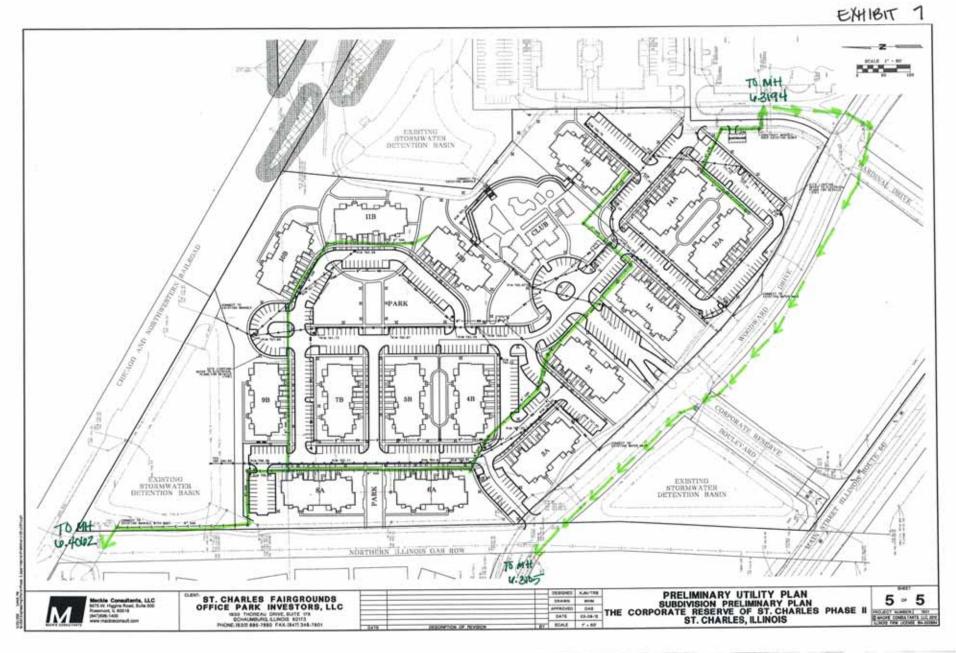
Upstream Manhole	Downstream Manhole	Upstream Elevation	Downstream Elevation	Pipe Length	Pipe Diameter	Pipe Slope	Pipe Capacity (CFS)	Cummulative Peak Sanitary Flow (CFS)	Total & (CFS)	Cummulative Wet Weather Flow (CFS)	Pipe Capacity (%)
6.3110	6.3109	748.79	747.56	114	8	1.08%	1.259	0.226	0.00410	0.230	18.2
6.3109	6.3108	747.56	746.07	125	8	1.19%	1.323	0.226	0.00410	0.234	17.7
6.3108	6.3107	746.07	745.57	126	8	0.40%	0.763	0.226	0.00410	0.234	30.6
6.3107	6.3106	745.57	742.99	162	8	1.59%	1.529	0.226	0.00410	0.234	15.3
6.3106	6.4063	742.99	741.70	137	8	0.94%	1.176	0.226	0.00410	0.234	19.9
6.4063	6.4062	741.70	740.50	129	8	0.93%	1.169	0.226	0.00410	0.234	20.0
6.4062	7.4049	735.18	734.99	87	12	0.22%	1.669	0.601	0.00410	0.609	36.5
7.4049	7.4048	734.99	734.30	180	12	0.38%	2.212	0.601	0.00410	0.609	27.5
7.4048	7.4047	734.30	734.14	43	12	0.37%	2.179	0.601	0.00410	0.609	27.9
7.4047	7.4046	734.14	733.62	167	12	0.31%	1.993	0.601	0.00410	0.609	30.5
7.4046	7.4045	733.62	733.02	184	12	0.33%	2.040	0.601	0.00410	0.609	29.8
7.4045	7.3094	733.02	732.75	114	12	0.24%	1.739	0.601	0.00410	0.609	35.0
7.3094	7.3090	732.75	732.16	132	12	0.45%	2.388	0.601	0.00410	0.609	25.5
7.3093	7.3092	746.22	745.07	118	8	0.97%	1.196	0.601	0.00410	0.609	50.9
7.3092	7.3091	745.07	740.60	116	8	3.85%	2.379	0.601	0.00410	0.609	25.6
7.3091	7.3090	740.60	737.63	85	8	3.49%	2.265	0.601	0.00410	0.609	26.9
7.3090	7.3083	737.63	731.72	202	12	2.93%	6.111	0.601	0.00410	0.609	10.0

Upstream Manhole	Downstream Manhole	Upstream Elevation	Downstream Elevation	Pipe Length	Pipe Diameter	Pipe Slope	Pipe Capacity (CFS)	Cummulative Peak Sanitary Flow (CFS)	Total & (CFS)	Cummulative Wet Weather Flow (CFS)	Pipe Capacity (%)
7.4002	7.4050	730.98	729.79	307	8	0.39%	0.754	0.255	0.00890	0.263	34.9
7.4050	7.3080	725.47	725.15	108	15	0.30%	3.526	0.255	0.00890	0.272	7.7
7.3080	7.3034	725.15	724.84	142	15	0.22%	3.026	1.073	0.01690	1.099	36.3
7.3034	7.3033	724.84	723.47	401	15	0.34%	3.786	1.073	0.01690	1.107	29.2
7.3033	7.3032	723.47	722.89	320	15	0.18%	2.758	1.073	0.01690	1.107	40.1
7.3032	7.3031	722.89	722.40	281	15	0.17%	2.705	1.108	0.01690	1.142	42.2
7.3031	7.3018	722.40	721.99	257	15	0.16%	2.587	1.108	0.01690	1.142	44.1
7.3018	7.3017	721.99	721.42	292	15	0.20%	2.862	1.564	0.03120	1.612	56.3
7.3017	7.3016	721.42	720.88	291	15	0.19%	2.790	1.564	0.03120	1.626	58.3
7.3016	7.3015	720.88	720.33	290	15	0.19%	2.821	1.564	0.03120	1.626	57.6
7.3015	7.3053	720.33	719.44	312	15	0.29%	3,459	1.564	0.03120	1.626	47.0

PROPOSED PEAK FLOW CALCULATIONS EXHIBIT 6

Manhole 6.3194 Sanitary Sewe	Manhole 6.3194 Sanitary Sewer Peak Flow PE 95 Peaking Factor 4.25 Peak Flow (Million Gallons Per Day) 0.040 Peak Flow (Gallons Per Day) 40371				
PE	95				
Peaking Factor	4.25				
Peak Flow (Million Gallons Per Day)	0.040				
Peak Flow (Gallons Per Day)	40371				
Flow (Gallons Per Minute)	28				
Flow (CFS)	0.062				

Manhole 6.4062 Sanitary Sewer Peak Flow					
Manhole 6.4062 Sanitary Sewe PE Peaking Factor Peak Flow (Million Gallons Per Day) Peak Flow (Gallons Per Day) Flow (Gallons Per Minute) Flow (CFS)	618				
Peaking Factor	3.93				
Peak Flow (Million Gallons Per Day)	0.242				
Peak Flow (Gallons Per Day)	242388				
Flow (Gallons Per Minute)	168				
Flow (CFS)	0.375				



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EXHIBIT 8

RENAUX MANOR

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PUMP STATION CALCULATIONS

PREPARED FOR:

WISEMAN-HUGHES ENTERPRISES 975 EAST 22nd STREET WHEATON, ILLINOIS 60187

PREPARED BY: INTECH CONSULTANTS, INC. 5413 WALNUT AVENUE DOWNERS GROVE, ILLINOIS 60515

> April 23, 1997 Revised June 27, 1997 Revised January 21, 1998

> > JOB NO. 95026

FLOW RATE CALCULATIONS

I. RENAUX MANOR FLOWS

• •

A. SINGLE FAMILY AREA

- 1. 265 units * 3.5 PE/unit = 927.5 PE
- 2. 927.5 PE * 100 gpcpd = 92,750 gpd (average)

B. MULTI-FAMILY AREA

- 1. 238 units * 3.0 PE/unit (assumed all 3 bedroom units) = 714 PE
- 2. 714 PE * 100 gpcpd = 71400 gpd (average)

C. COMMERCIAL SITE

- 1. 7.6 acres * 15 PE/ acre = 114 PE
- 2. 114 PE * 100 gpcpd = 11400 gpd (average)

II. OFFSITE FLOWS

- A. AREA TRIBUTARY TO MANHOLE 46 (RHA&A plans) MINUS RENAUX MANOR AREA
 - 1. 2747 PE (manhole 46) 612 PE (from Renaux Manor) + 70 PE (from Area 2) = 2205 PE
 - 2. 2205 PE * 100 gpcpd = 220500 gpd (average)
- B. AREA TRIBUTARY TO MANHOLE 33 (RHA&A plans) MINUS RENAUX MANOR AREA
 - 2422 PE (manhole 33) 582 PE (from Renaux Manor) 70 PE (from Renaux Manor) - 1740 PE (from water treatment plant, per Greg Chismark, City of St. Charles) = 30 PE
 - 2. 30 PE * 100 gpcpd = 3000 gpd (average)

III. TOTAL FLOW TO LIFT STATION

- A. [927.5 + 714 + 114 (Renaux Manor)] + [2205 + 30 (offsite area)] = 3990.5 PE use 4000 PE
- B. Average flow: 4000 PE * 100 gpcpd = 400,000 gpd = 277.7 gpm

C. Calculated peaking factor = $(18 + (4^{-5}))/(4+(4^{-5})) = 3.33$

- D. Q max. using 3.33 peaking factor = 1,333,333 gpd calculated max = 925 gpm
- E. Q max. using 4.0 peaking factor = 1,600,000 gpd design maximum = 1111 gpm 1111 gpm flow used for lift station design

1	Tributary To Renoux Manor Lift Station: Existing Condition Residentia						
Area	Manhole Location	Single Family Units	Multi Family Units	Flow Per Unit (GPD)	Total Flow (GPD)		
Renaux Manor Unit 1 & Artesian Springs	7.3018	152	-	350	53,200		
Renaux Manor Unit 2 ²	To Lift Station	-	35	1200	42,000		
Renaux Manor Unit 2 ²	7.3018	-	29	1200	34,800		
Renaux Manor Unit 3	7.4002	117	-	350	40,950		
Remington Glen ¹	7.3083	-	26	-	36,050		
Autumn Leaves Assisted Living ¹	7.3081	-	1	6000	6,000		
Pine Ridge & Regency Estates ¹	To Lift Station	-	-	-	56,900		
Assisted Living ³	To Lift Station	-	1	12000	12,000		
	Total Da	ily Flow for Residential			281,900		

Notes:

1) Total flow value based on information obtained from IEPA permit supplied by the City of St. Charles

2) Renaux Manor Unit 2: 1 Multi Family Unit = 4 3-BR units. See calculation sheet for breakdown of flow per unit (gpd)

3) Assisted Living: Complex located off of IL Rt 64. Estimated flow (gpd) based on two times the value of Autumn Leaves Assisted Living

······································	Tributary To Renoux Manor Lift Station: Existing Condition Non-Residentia								
Building	Manhole Location	Use	Acres	Employees or PE/acre	GPD/Employee (GPD)	Total Flow (GPD)			
Walgreens ^{2,4}	7.3032	Commercial	-	73	15.00	1,095			
Corporate Reserve - north ³	6.3196	Office Buildings	0.4	70	15.00	1,045			
Corporate Reserve - central ³	6.3198	Office Buildings	0.4	70	15.00	1,045			
Corporate Reserve - south ³	6.3194	Office Buildings	0.6	105	15.00	1,568			
Corporate Reserve - vacant west ¹	6.3192	Commercial	4.2	20	-	8,400			
Corporate Reserve - vacant east ¹	6.3189	Commercial	3.3	20	-	6,600			
Vacant Lot ¹	6.3105	Commercial	2.0	20	-	3,960			
Valley Springs Auto ²	7.3032	Commercial	-	-	-	3,000			
Main Street Center ²	7.3087	Office Buildings	-	-	-	3,200			
Westgate ²	7.3032	Commercial	-	-		2,400			
The Bike Rack & Adjacent Commercial ³	To Lift Station	Commercial	0.8	132	15	1,986			
Fire Station ³	To Lift Station	-	0.2	35	15	523			
		Total Daily Flows for N	on-Residential			34,823			

Notes:

1) Area in acres measured by planimeter. 20 PE/acre used as conservative estimate for projected future use

2) PE value taken from issued IEPA permits supplied by the City of St. Charles

3) Number of employees based on 1 person per 250 square feet

4) Total flow based on IEPA permit; 73 estimated employees

Tributary To Reno	ux Manor Lift Station	: Proposed Condit	tion Residential (Co	orporate Reserve of St.	. Charles Ph II
Area	Manhole Location	Single Family Units	Multi Family Units	Flow Per Unit (GPD)	Total Flow (GPD)
Corporate Reserve - proposed	6.4062	-	13	4750	61,750
Corporate Reserve - proposed	6.3194	-	2	4750	9,500
	Total Da	ily Flow for Residential			71,250

Notes:

1) 1 Multi Family Unit = 1 studio, 11-1BR, 10-2BR units. See calculation sheet for breakdown of flow per unit (gpd)

Summary of Average Daily Flows into Renaux Manor Lift Station					
	GPD				
Existing Condition Residential	281,900				
Existing Condition Non-Residential	34,823				
Proposed Condition Residential	71,250				
TOTAL	387,973				

SUPPORTING DOCUMENTS

Wills Burke Kelsey Associates, Ltd. 116 West Main Street, Suite 201, St. Charles, Illinois 60174 TEL: (630) 443-7755 FAX: (630) 443-0533 8 East Galena Boulevard, Suite 402, Aurora, Illinois 60506 TEL: (630) 701-2245 FAX: (630) 800-1626

JOB 12-0120 SHEET NO. OF . CALCULATED BY DATE CHECKED BY _ DATE SCALE

Average Flow per Multi Family Blog & Coeporate Reserve avg units per building = 22 #Studio F #1.BRT \$2HC= 22 Units BRIGHION Equivalent (PE) Studio = 1 persons 1 BR = 1.5 persons - 7 2 RR = 3 persons - 7 100 gpd 1- studio (IPE) + 11-18R\$ (1.5PE) + 10-2ER\$ (3PE) = 41.56 41.5 PE (100 gpd) = 4150 gpd building Renaux Manor Unit avg units per building = 4, assume all BBR (PE=3) $3PE \times 4 units = 12PE$ 12PE(100gpa) = 1200gpd/building

INSTRUCTIONS FOR SCHEDULE A -- SEWER SERVICE CONNECTIONS OR SCHEDULE B - PUBLICLY OWNED OR REGULATED SEWER EXTENSIONS Revised November 2005

Schedule A must be filled out and completed for all sewer connections, which must be covered by a permit in accordance with the Illinois Pollution Control Board Regulations or where the municipality or local public sewer owner will not provide maintenance on said sewer. Sewer extensions which are to be maintained by the municipality or local sewer owner use Schedule B.

When the schedule item is not applicable to your project write "not applicable" or N/A.

- 1. The name of the project must be the same as the project name indicated on Form WPC-PS-1.
- 2. The sewer connection or non-public sewer will serve the indicated type of user such as the residential, commercial, light industrial (domestic only), manufacturing, recreational, other. It may be possible that one, two, or all of the appropriate blanks would be checked as well.
- 3. The nature of the project is intended to be a brief summary description of the type of project covered by the permit application.
- 4.1. Either submit the required map or a letter from the Illinois Historic Preservation Agency indicating that they have reviewed the project. The Agency has committed to a cooperative effort with the Illinois Historic Preservation Agency (IHPA). Under the provisions of the State Agency Historic Resources Preservation Act, 30 ILCS 605/1, IEPA informs IHPA of construction permit applications shortly after they are received. We would appreciate your submission of location maps and legal descriptions to facilitate this process. IEPA is obligated not to issue the permit until 30 days from the date that IHPA has received the copy of the application or until a letter is received from them. Permit applicants should submit information to IHPA independently from applying for construction permits from IEPA. If the project has previously been reviewed by the Illinois Historic Preservation Agency, inclusion of the sign off letter or approval with your application will enable IEPA to process your application more expeditiously. IHPA contact information is:

ILLINOIS HISTORIC PRESERVATION AGENCY Division of Review and Compliance 1 Old State Capitol Plaza Springfield, Illinois 62701
 Telephone Number:
 217/785-4512

 Fax Number:
 217/782-8161

- 4.2. Please submit a sketch of the project. If a suitable clear layout is included on the plan drawings, this request will be considered met.
- 4.3. A map of the immediate area to be served by the sewer in question must be submitted.
- 4.4. All potential future service area must also be shown.

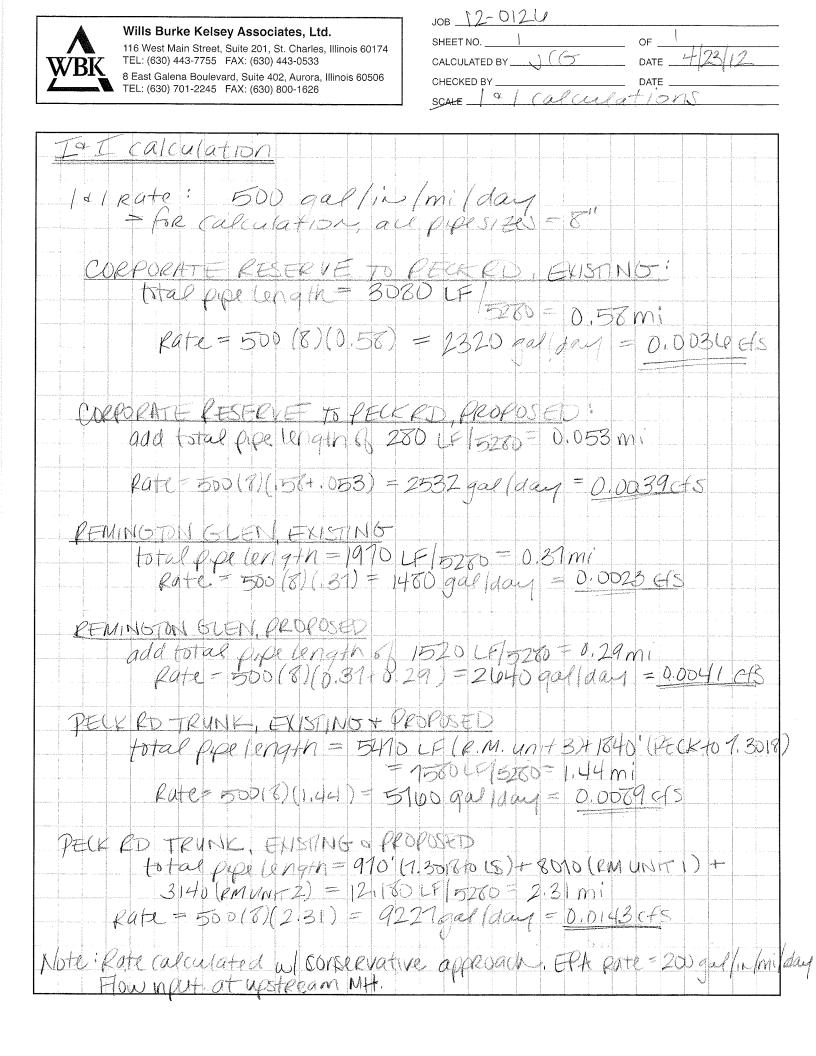
It should be emphasized that the loading allocated against the waste treatment facility and intermediate sewer system will be based on the immediate area and population to be served by the permit. Any review fee for this project (see 6.4 below) will be based on the design loading of the sewer.

- 5. A facilities planning area (FPA) is a defined area that anticipates sewer service to be provided by a specific wastewater treatment facility. This information should be available from the owner/operator of the sewerage system or the owner of the sewage treatment plant. Sewers serving areas not identified in the proper FPA will be denied.
- 6. The following design criteria should be used in estimating the population equivalent of a residential building:

Efficiency or Studio Apartment	= 1	person
1 Bedroom Apartment	= 1.5	persons
2 Bedroom Apartment	= 3	persons - ALSO USE FOR TOWNTHOME
3 Bedroom Apartment	= 3	persons - ALSO USE FURN TURN
Single Family Home	= 3.5	persons
Mobile Home	= 2.25	persons

Commonly used quantities of sewage flows from miscellaneous type facilities are listed in Appendix B, Table No. 2 of the Illinois Recommended Standards for Sewage Works.

6.3 Total of Items 6.1 and 6.2.



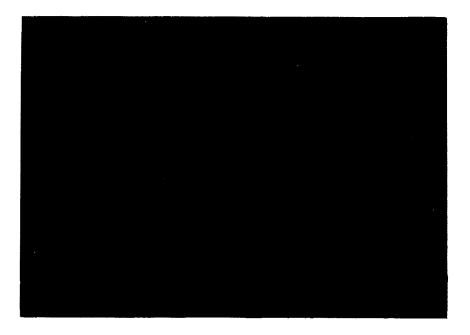


Wills Burke Kelsey Associates, Ltd.

116 West Main Street, Suite 201, St. Charles, Illinois 60174 TEL: (630) 443-7755 FAX: (630) 443-0533 8 East Galena Boulevard, Suite 402, Aurora, Illinois 60506 TEL: (630) 701-2245 FAX: (630) 800-1626

JOB 12-0120 SHEET NO. OF _ CALCULATED BY_ DATE _ CHECKED BY DATE SCALE

Avreage Daily Flow per feat time pump data Hump (apacity = 040 gpm (per specs) average daily pump time = 12 hes (pee data from) an 2012 - Mae 2012) 690 gal, 1.2 hes (00 min = 49,080 gallons 2 pumps = 49,000 gal × 2 = 99,360 gal * third pump run time data suggests it is not utilized average daily flow - 99.360 gal/day that Flow per real time pump data fump capacity = 690 gpm peak pump time = 3.7 hrs (Van 2012) $U_{m,n}^{a} = \frac{3.1}{100} + \frac{100}{100} = 153,180$ 99/1005 2 pumps × 153,180 gel = 304, 300 gal/day



Metropolitan Industries, Inc.

Metropolitan Pump Company

Metropolitan Marketing

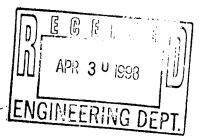
Metropolitan Equipment

MANUFACTURERS & DISTRIBUTORS OF QUALITY EQUIPMENT

Metropolitan Industries, Inc. SUBMISSION FOR APPROVAL

ł

PROJECT TRIPLEX COMPONENT LIFT STATION



LOCATION

RENAUX MANOR ST. CHARLES, ILLINOIS

ENGINEER

INTECH CONSULTANTS

CONTRACTOR DEMPSY ING

REPRESENTATIVE ROBERT L. WEDELL

> **DATE** April 28, 1998

Specifications

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PROJECT:	Sanitary Lift Station Renaux Manor St. Charles, Illinois
Application:	Triplex Component Lift Station
Model:	(3) Hydromatic model S4BX750 submersible non-clog explosion proof sewage pumps with 75' dual cords.
Capacity:	690 GPM @ 29' TDH 3" dia. solids / 4" discharge
Motor(s):	(2)7 1/2HP, 1150 RPM, 460 volt, 3 phase 60 Hz., 1.20 service factor Explosion Proof: Class I, Division I, Group C and or D Locations
Control:	 (1) Submersible level transducer (primary) (5)Submersible mercury level switches to control on, off, override and alarm levels (secondary). All with 75' cords.
Control Panel:	Furnished Control panel to include magnetic starters, circuit breakers, run lights, H-O-A switches, electric alternator, main disconnect switch, ETM's, heat and seal failure sensors, intrinsically safe relays, automatic transfer switch (by Patton Power), Level Master and variable frequency drives all in a NEMA 3R "traffic box" type enclosure.
Alarm:	High water alarm light & AUTOMATTE OONNECTION TO MANN CONTROL 10' dia X 33 13' doop with outpide value hav
Basin:	10' dia. X 33.13' deep with outside valve box Concrete, piping and valves - by others
	 3) Simplex Aluminum wet well access hatch model: APS300-36x32 (1) Simplex aluminum valve vault access hatch model APS300-36x36 (3) 4" M-T-M base elbows (3) 4" M-T-M seal flanges (3) 33' lengths of 3/16" stainless steel lifting chain (12) 17' lengths of 2" sched. 40 stainless steel guide rails (3) Sets of lower guide rail supports (located on base elbow) (3) Sets of intermediate guide rail supports (3) Sets of upper guide rail supports (mounted to wet ell access hatches) (1) Stainless steel 5 float mounting bracket (2) 10 lbs cast iron anchor and stainless steel chain float mounting system (1) Heat and seal failure probes (per pump)
	METROPOLITAN PUMP COMPANY division of Metropolitan Industrios, Inc.

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37 Forestwood Drive Romeoville, Illinois 60446 phone: (815)886-9200 fax: (815)886-4573

Jan. 2012	Pump #1		Pump #2		Pump #3	
Date	Hour Meter	Hours Run	Hour Meter	Hours Run	Hour Meter	Hours Run
1	6169.9	0.0	7994.9	0.0	9294.9	0.0
2	6169.9	3.4	7994.9	0.0	9294.9	2.6
3	6173.3	1.4	7994.9	0.0	9297.5	1.1
4	6174.7	1.2	7994.9	0.0	9298.6	0.9
5	6175.9	1.4	7994.9	0.0	9299.5	1.1
6	6177.3	0.0	7994.9	0.0	9300.6	0.0
7	6177.3	2.5	7994.9	0.0	9300.6	1.9
8	6179.8	0.0	7994.9	0.0	9302.5	0.0
9	6179.8	3.3	7994.9	0.0	9302.5	2.6
10	6183.1	1.4	7994.9	0.0	9305.1	1.1
11	6184.5	1.1	7994.9	0.0	9306.2	0.8
12	6185.6	1.5	7994.9	0.0	9307.0	1.2
13	6187.1	0.0	7994.9	0.0	9308.2	0.0
14	6187.1	2.4	7994.9	0.0	9308.2	1.9
15	6189.5	1.4	7994.9	0.0	9310.1	1.6
16	6190.9	0.0	7994.9	0.0	9311.7	0.0
17	6190.9	2.2	7994.9	0.0	9311.7	3.1
18	6193.1	1.0	7994.9	0.0	9314.8	1.3
19	6194.1	0.9	7994.9	0.0	9316.1	0.0
20	6195.0	0.0	7994.9	0.0	9316.1	0.0
21	6195.0	1.8	7994.9	0.0	9316.1	3.7
22	6196.8	1.4	7994.9	0.0	9319.8	2.0
23	6198.2	0.0	7994.9	0.0	9321.8	0.0
24	6198.2	2.4	7994.9	0.0	9321.8	3.3
25	6200.6	0.8	7994.9	0.0	9325.1	1.0
26	6201.4	1.1	7994.9	0.0	9326.1	1.6
27	6202.5	0.0	7994.9	0.0	9327.7	0.0
28	6202.5	2.5	7994.9	0.0	9327.7	2.0
29	6205.0	1.9	7994.9	0.0	9329.7	1.5
30	6206.9	0.0	7994.9	0.0	9331.2	0.0
31	6206.9	0.0	7994.9	0.0	9331.2	0.0
Carried Forward	6206.9		7994.9		9331.2	
Total		37.0		0.0		36.3
Daily Avg.		1.2		0.0		1.2
Daily Max.		3.4		0.0		3.7

Feb. 2012	Pump #1		Pump #2		Pump #3		
Date	Hour Meter	Hours Run	Hour Meter	Hours Run	Hour Meter	Hours Run	
1	6209.8	1.2	7994.9	0.0	9333.4	1.0	
2	6211.0	1.5	7994.9	0.0	9334.4	1.2	
3	6212.5	0.0	7994.9	0.0	9335.6	0.0	
4	6212.5	2.6	7994.9	0.0	9335.6	2.0	
5	6215.1	2.0	7994.9	0.0	9337.6	1.6	
6	6217.1	0.0	7994.9	0.0	9339.2	0.0	
7	6217.1	2.7	7994.9	0.0	9339.2	2.2	
8	6219.8	0.9	7994.9	0.0	9341.4	0.8	
9	6220.7	1.8	7994.9	0.0	9342.2	1.5	
10	6222.5	0.0	7994.9	0.0	9343.7	0.0	
11	6222.5	2.5	7994.9	0.0	9343.7	1.9	
12	6225.0	1.4	7994.9	0.0	9345.6	1.8	
13	6226.4	0.0	7994.9	0.0	9347.4	0.0	
14	6226.4	2.2	7994.9	0.0	9347.4	3.0	
15	6228.6	0.8	7994.9	0.0	9350.4	1.1	
16	6229.4	1.1	7994.9	0.0	9351.5	1.5	
17	6230.5	0.0	7994.9	0.0	9353.0	0.0	
18	6230.5	2.1	7994.9	0.0	9353.0	2.9	
19	6232.6	1.7	7994.9	0.0	9355.9	1.3	
20	6234.3	0.0	7994.9	0.0	9357.2	0.0	
21	6234.3	2.4	7994.9	0.0	9357.2	2.5	
22	6236.7	0.9	7994.9	0.0	9359.7	1.2	
23	6237.6	1.4	7994.9	0.0	9360.9	1.6	
24	6239.0	0.0	7994.9	0.0	9362.5	0.0	
25	6239.0	2.8	7994.9	0.0	9362.5	2.8	
26	6241.8	0.5	7994.9	0.0	9365.3	1.8	
27	6242.3	0.0	7994.9	0.0	9367.1	0.0	
28	6242.3	2.2	7994.9	0.0	9367.1	3.1	
29	6244.5	0.0	7994.9	0.0	9370.2	0.0	
Carried Forward	6244.5		7994.9		9370.2		
Total		34.7		0.0	•	36.8	
Daily Avg.		1.2		0.0		1.3	
Daily Max.		2.8		0.0		3.1	

Mar. 2012	Pump #1		Pump #2		Pump #3	
Date	Hour Meter	Hours Run	Hour Meter	Hours Run		Hours Run
1	6245.5	0.8	7994.9	0.0		0.7
2	6246.3	0.0	7994.9	0.0	9372.2	0.0
3	6246.3	1.9	7994.9	0.0	9372.2	3.0
4	6248.2	1.4	7994.9	0.0	9375.2	1.9
5	6249.6	0.0	7994.9	0.0	9377.1	0.0
6	6249.6	2.2	7994.9	0.0	9377.1	3.1
7	6251.8	0.7	7994.9	0.0	9380.2	1.0
8	6252.5	1.2	7994.9	0.0	9381.2	1.6
9	6253.7	0.0	7994.9	0.0	9382.8	0.0
10	6253.7	1.8	7994.9	0.0	9382.8	2.8
11	6255.5	1.4	7994.9	0.0	9385.6	1.6
12	6256.9	0.0	7994.9	0.0	9387.2	0.0
13	6256.9	2.2	7994.9	0.0	9387.2	3.0
14	6259.1	1.1	7994.9	0.0	9390.2	1.6
15	6260.2	0.8	7994.9	0.0	9391.8	1.2
16	6261.0	0.0	7994.9	0.0	9393.0	0.0
17	6261.0	2.0	7994.9	0.0	9393.0	2.7
18	6263.0	1.3	7994.9	0.0	9395.7	1.8
19	6264.3	0.0	7994.9	0.0	9397.5	0.0
20	6264.3	2.0	7994.9	0.0	9397.5	2.8
21	6266.3	1.3	7994.9	0.0	9400.3	1.7
22	6267.6	0.8	7994.9	0.0	9402.0	1.1
23	6268.4	0.0	7994.9	0.0	9403.1	0.0
24	6268.4	1.8	7994.9	0.0	9403.1	2.6
25	6270.2	1.3	7994.9	0.0	9405.7	1.8
26	6271.5	0.0	7994.9	0.0	9407.5	0.0
27	6271.5	1.8	7994.9	0.0	9407.5	2.5
28	6273.3	0.9	7994.9	0.0	9410.0	1.2
29	6274.2	1.0	7994.9	0.0	9411.2	1.4
30	6275.2	0.0	7994.9	0.0	9412.6	0.0
31	6275.2	0.0	7994.9	0.0	9412.6	0.0
Carried Forward	6275.2		7994.9		9412.6	
Total		29.7		0.0		41.1
Daily Avg.		1.0		0.0		1.3
Daily Max.		2.2		0.0		3.1



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WILLS BURKE KELSEY ASSOCIATES

MEMORANDUM

Date: May 7, 2012

To: Chris Tiedt P.E.

CC:

From: Greg Chismark

Subject: Corporate Reserve Sanitary Sewer Study

This memo is a follow up to the subject study at the request of City staff. The purpose is to document the projected wastewater flow from the Corporate Reserve development (former Cardinal Property) comparing several sources. These are:

- Improvements Phasing Plan Update for Fairgrounds / West Gateway Development dated January 1996
- West Side WRF Facility Plan Update dated August 2008
- Corporate Reserve of St. Charles Sanitary Sewer Evaluation dated April 2012

The Corporate Reserve development is located on the former Cardinal Property. Generally, it is located between IL Route 64 (Main Street) and the former UPRR tracks / Great Western Trail and Remington Glen and Regency Estates / Pine Ridge Park. The entire property consists of approximately 50 acres. Find below a table comparing projected wastewater flows.

Source	Est P.E.	Flow gpd	Land Use	Comments
Improvements Phasing Plan Fairgrounds/West Gateway - 1996	903	90,300	Mixed	Significant residential component @ 24 P.E./ac.
West Side WRF Facility Plan Update- 2008	500	50,000		10 P.E./ac.
Corporate Reserve Sanitary Sewer Study - 2012	899	89,908	Mixed	Office/ commercial & proposed multi-unit residential

It is noted that the 2012 flows and the 1996 flows are similar in magnitude. However, the 2008 flows are significantly less. Most likely this is a result of the land use proposed (or approved) at the time the study was prepared and may be based on the assumption that a majority of the property will be an office use.



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WILLS BURKE KELSEY ASSOCIATES

MEMORANDUM

Date: May 21, 2012

To: Chris Tiedt P.E.

CC: James Bernahl P.E.

From: Greg Chismark

Subject: Corporate Reserve Sanitary Sewer Study

This memo is in response to City staff comments regarding the sanitary sewer evaluation for the Corporate Reserve project. The goal of this supplement is to take a more refined look at the wastewater flows generated from the Corporate Reserve site. Although we took a conservative approach, City staff is concerned that the clubhouse and pool area has not been specifically accounted for in the analysis. The following documents were utilized:

- Improvements Phasing Plan Update for Fairgrounds / West Gateway Development dated January 1996
- Clubhouse Floor Plan prepared by BSB Design dated March 19, 2012
- Title 35 of the Illinois Administrative Code Part 370 Recommended Standards for Sewage Works
- Title 15A North Carolina Administrative Code Wastewater Design Flow Rates

Upon evaluation of the clubhouse floor plan we identified three separate uses. These uses include the pool, the social room/fitness room and the office area. We have assumed these uses would occur daily and throughout the year. This is a very conservative assumption but a good starting point. The flow generate rates were taken from both the Illinois and North Carolina Administrative Codes. The North Carolina Administrative Code was utilized to establish a flow rate for the pool and fitness areas because the Illinois Administrative Code does not address these uses. The estimated flow rate for the clubhouse facility is 2,100 gpd or 21 P.E.

We also verified the residential unit count and flows. Based on a rounding error the entire residential component could generate 72,100 (721 P.E) in comparison to the 71,250 (712.5 P.E.) originally estimated. This is an increase of 850 gpd or 8.5 P.E.

Finally, we re-evaluated the 7.5 acres of vacant commercial land use adjacent to Main Street (IL 64). The original estimate used a very conservative flow generation rate of 20 P.E./acre. This is 5 P.E./acre greater than the rate used in the original Fairgrounds / West Gateway Development Improvements Phasing Plan. It is reasonable to adjust flow rates for the commercial areas utilizing the original flow generation rates. The resultant is a reduction of 3,750 gpd or 37.5 P.E.

Taking into account all the afore-noted adjustments to total flow from the project can be reduced by 800 gpd or 8 P.E. We recommend the originally calculated flow rates and analysis remain unchanged as a conservative approach.

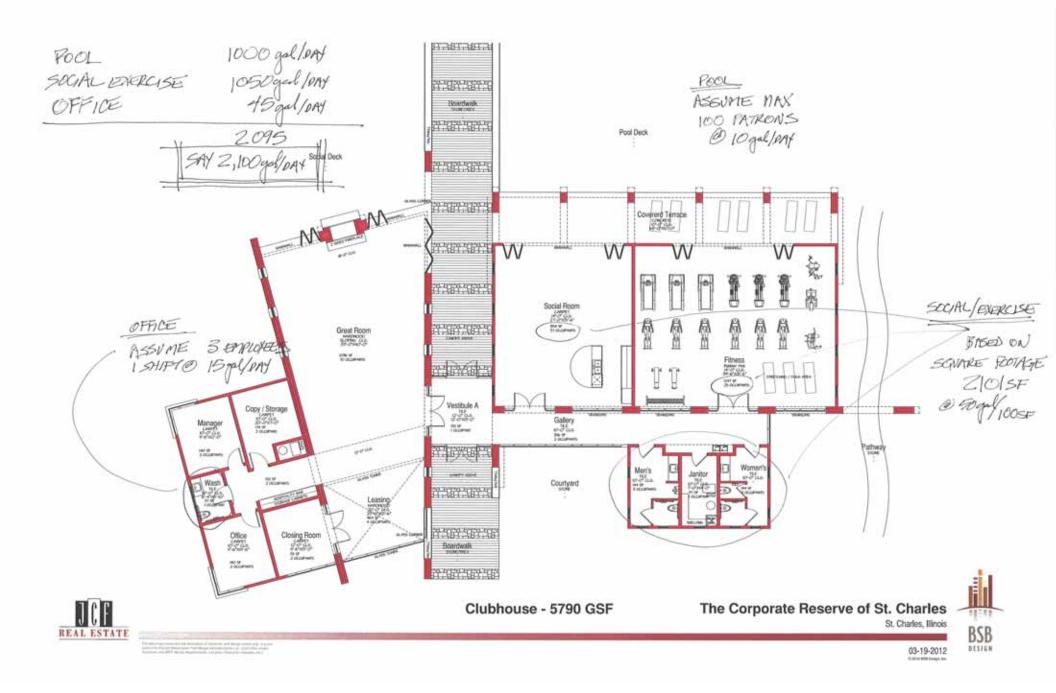


EXHIBIT 9

Area	Manhole Location	Single Family Units	Multi Family Units	Flow Per Unit (GPD)	Total Flow (GPD)
Renaux Manor Unit 1 & Artesian Springs	7.3018	152		350	53,200
Renaux Manor Unit 2 ²	To Lift Station		35	1200	42,000
Renaux Manor Unit 2 ²	7.3018	-	29	1200	34,800
Renaux Manor Unit 3	7,4002	117		350	40,950
Remington Glen ¹	7.3083		26		36,050
Autumn Leaves Assisted Living ¹	7.3081		1	6000	6,000
Pine Ridge & Regency Estates ¹	To Lift Station	+			56,900
Assisted Living [®]	To Lift Station		1	12000	12,000
Total Daily Flow for Residential					

Notes:

1) Total flow value based on information obtained from IEPA permit supplied by the City of St. Charles

2) Renaux Manor Unit 2: 1 Multi Family Unit = 4 3-BR units. See calculation sheet for breakdown of flow per unit (gpd)

3) Assisted Living: Complex located off of IL Rt 64. Estimated flow (gpd) based on two times the value of Autumn Leaves Assisted Living

Building	Manhole Location	Use	Acres	Employees or PE/acre	GPD/Employee (GPD)	Total Flow (GPD)	A
Walgreens ^{2,4}	7.3032	Commercial		73	15.00	1,095	
Corporate Reserve - north*	6.3196	Office Buildings	0.4	70	15.00	1,045	
Corporate Reserve - central ¹	6.3198	Office Buildings	0.4	70	15.00	1,045	
Corporate Reserve - south	6.3194	Office Buildings	0.6	105	15.00	1,568	
Corporate Reserve - vacant west ¹	6.3192	Commercial	4.2	20- 15		8,400	6,300
Corporate Reserve - vacant east ¹	6.3189	Commercial	3.3	30-15	-	6,600	4,990
Vacant Lot ¹	6.3105	Commercial	2.0	20		3,960	0700
Valley Springs Auto ²	7.3032	Commercial		+	-	3,000	A= - 5190 g
Main Street Center ²	7,3087	Office Buildings			-	3,200	Δ= - 3750 g 3759 g
Westgate ²	7.3032	Commercial			-	2,400	2760
The Bike Rack & Adjacent Commercial ³	To Lift Station	Commercial	0.8	132	15	1,986	71.74
Fire Station ¹	To Lift Station	-	0.2	35	15	523	
Total Daily Flows for Non-Residential						34,823	1

Notes:

1) Area in acres measured by planimeter. 20 PE/acre used as conservative estimate for projected future use

2) PE value taken from issued IEPA permits supplied by the City of St. Charles

3) Number of employees based on 1 person per 250 square feet

4) Total flow based on IEPA permit; 73 estimated employees

Area	Manhole Location	Single Family Units	Multi Family Units	Flow Per Unit (GPD)	Total Flow (GPD)
Corporate Reserve - proposed	6.4062		13	4750	61,750
Corporate Reserve - proposed	6.3194		2	4750	9,500

Notes:

1) 1 Multi Family Unit = 1 studio, 11-1BR, 10-2BR units. See calculation sheet for breakdown of flow per unit (gpd)